

K

Nr *II 112*
Politechnika Warszawska

BULLETIN
DE
L'ACADÉMIE POLONAISE
DES SCIENCES

SÉRIE DES SCIENCES TECHNIQUES

Volume XII, Numéro 11a (Supplément)

PROBLÈMES NON-CLASSIQUES DES
VOILES MINCES

Symposium IASS, Varsovie, 1963

VARSOVIE 1964

Thermal Stresses in Elastic and Viscoelastic Shells

by
W. NOWACKI

The purpose of the present paper is to determine the displacements produced in shells by a field of initial deformations (distortions), in particular by the field of temperature. The starting point for our considerations is the reciprocal theorem for a three-dimensional elastic body, distortions being taken into account. This theorem will be specialized to the plane state of stresses in shells. The theorem in three-dimensional state of stresses assumes the form [1], [2]:

$$(1.1) \quad \int_V X'_i u''_i dV + \int_S p'_i u''_i dS + \int_V \varepsilon^{0'}_{ij} \sigma''_{ij} dV = \int_V X''_i u'_i dV + \int_S p''_i u'_i dS + \\ + \int_V \varepsilon^{0''}_{ij} \sigma'_{ij} dV, \\ i, j = 1, 2, 3.$$

In the above equation there appear two states denoted correspondingly by "prime" and "double prime". Thus, in the first state u'_i denote the components of displacement vector \vec{u}' ; X'_i are the components of the body forces vector \vec{X}' , while p'_i are the components of the vector of surface loadings \vec{p}' ; σ'_{ij} denote the stress tensor components and $\varepsilon^{0'}_{ij}$ are the distortion components. λ and μ are the Lamé constants. The integration is performed over volume V and surface S bounding an elastic body.

Let us consider an elastic body clamped on the part S_1 of the region S and on the remaining part S_2 free from loadings. Suppose the required displacements u'_i to be produced by distortions $\varepsilon^{0'}_{ij}$. We assume that $X'_i = 0$. As the second state of loading we assume the concentrated unit force acting at point (ξ) and directed along the x_k axis. Moreover, let $\varepsilon^{0''}_{ij} = 0$. Substituting in (1.1) $X'_i = 0$, $\varepsilon^{0''}_{ij} = 0$, and

$$X''_i = \delta(x_1 - \xi_1) \delta(x_2 - \xi_2) \delta(x_3 - \xi_3) \delta_{ik},$$

and taking into account that the surface integrals vanish, we obtain:

$$(1.2) \quad 1''_k u'_k(\xi) = \int [2\mu \varepsilon^{0'}_{ij}(x) \varepsilon^{''(k)}_{ij}(x, \xi) + \lambda e^{0'}(x) e^{''(k)}(x, \xi)] dV(x), \\ i, j, k = 1, 2, 3.$$

Deformations $\varepsilon^{''(k)}_{ij}(x, \xi)$ and dilatation $e^{''(k)}(x, \xi)$ are Green functions; they denote the deformations and the dilatation at point (x) produced by the action of

the concentrated force applied at (ξ) and directed along the x_k axis. Eq. (1.2) may be written also in the following form:

$$(1.3) \quad u'_k(\xi) = \int_V \varepsilon_{ij}^0(x) \sigma_{ij}^{\prime\prime(k)}(x, \xi) dV(x), \quad i, j, k = 1, 2, 3,$$

where the components of the stress state produced by the action of the concentrated force at point (ξ) and directed along the x_k axis are denoted by $\sigma_{ij}^{\prime\prime(k)}(x, \xi)$.

The stresses $\sigma_{ij}^{\prime\prime(k)}$ are given by the formulae

$$(1.4) \quad \sigma_{ij}^{\prime\prime(k)} = 2\mu(\gamma_{ij}^{(k)} + x_3 \kappa_{ij}^{(k)}) + \eta \delta_{ij}(\gamma^{(k)} + x_3 \kappa^{(k)}),$$

$$\gamma^{(k)} = \gamma_{jj}^{(k)}, \quad \kappa^{(k)} = \kappa_{jj}^{(k)}, \quad \eta = \frac{2\mu\lambda}{\lambda + 2\mu}.$$

Suppose that distortions ε_{ij}^0 are linear functions of x_3

$$(1.5) \quad \varepsilon_{ij}^0 = \psi_{ij}^0 + x_3 \varphi_{ij}^0, \quad \psi_{ij}^0 \equiv \psi_{ij}^0(x_1, x_2), \quad \varphi_{ij}^0 \equiv \varphi_{ij}^0(x_1, x_2).$$

If we substitute (1.5) into (1.3) and make use of relations (1.4), then performing the integration with respect to x_3 , we obtain the following formulae for, displacement:

$$(1.6) \quad u_k(\xi_1, \xi_2) = \int \int_{(r)} [\psi_{ij}^0(x_1, x_2) N_{ij}^{(k)}(x_1, x_2, \xi_1, \xi_2) + \\ + \varphi_{ij}^0(x_1, x_2) M_{ij}^{(k)}(x_1, x_2, \xi_1, \xi_2)] dx_1, dx_2$$

Here, $N_{ij}^{(k)}$ denote the normal and shear forces, $M_{ij}^{(k)}$ — the bending moments and torques produced in the shell by the action of the concentrated force at point (ξ) and directed along the x_k axis.

This method of solution briefly outlined above may be extended on the problems of shells and even — making use of the elastic-viscoelastic analogy — on the viscoelastic shells.

In the final part an example is given relating to the thermal stresses in an open cylindrical shell.

INSTITUTE OF FUNDAMENTAL TECHNICAL PROBLEMS, POLISH ACADEMY OF SCIENCES, WARSAW (POLAND)

REFERENCES

- [1] V. M. Maysel, *Generalization of Betti-Maxwell theorem on the case of thermal stresses and some applications of this generalization* [in Russian], Dokl. AN, SSSR, **30** (1941), No. 2.
- [2] W. Nowacki, *Thermal stresses in anisotropic bodies* [in Polish], Arch. Mech. Stos., **6** (1954), No. 3.
- [3] T. Alfrey, *Nonhomogeneous stresses in viscoelastic media*, Quart. Appl. Math., **2** (1944).
- [4] E. H. Lee, *Stress analysis in viscoelastic bodies*, Quart. Appl. Math., **8** (1955), No. 2.
- [5] L. H. Donnell, *Stability of thin-walled tubes under torsion*, NACA, T.R. 479, 1933.