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A Plane Dynamic Distortion Problem in Stresses

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Let us consider an elastic body subjected to initial stresses produced by a distortional field characterized by initial strains ε_{11}^0 , ε_{22}^0 , ε_{33}^0 , ε_{12}^0 , depending on the coordinates x_1, x_2 and time t .

In order to determine the stress components σ_{ij} and the strain components ε_{ij} , we make use of the dynamic stress functions. This way is particularly useful in the case when the external loadings are given or for a cylinder free from stresses on its curved surface. For the plane strain state the relations between the stresses σ_{ij} , strains ε_{ij} and distortions ε_{ij}^0 are given by the equations

$$(1) \quad \sigma_{ij} = 2\mu(\varepsilon_{ij} - \varepsilon_{ij}^0) + \lambda\delta_{ij}(e - \bar{e}^0), \quad i, j = 1, 2,$$

$$(2) \quad \sigma_{33} = -2\mu\varepsilon_{33}^0 + \lambda(e - \bar{e}^0), \quad e = \varepsilon_{11} + \varepsilon_{22}, \quad \bar{e}^0 = \varepsilon_{11}^0 + \varepsilon_{22}^0 + \varepsilon_{33}^0.$$

We assume that the plane strain state $(\varepsilon_{11}, \varepsilon_{22}, \varepsilon_{12}) \neq 0$ is produced by the state $(\varepsilon_{11}^0, \varepsilon_{22}^0, \varepsilon_{12}^0, \varepsilon_{33}^0) \neq 0$ and by a surface loading.

In Eqs. (1), (2) μ, λ are the Lamé constants and δ_{ij} is the Kronecker delta. The strains ε_{ij} ($i, j = 1, 2$) are connected with the displacements by the relations

$$(3) \quad \varepsilon_{ij} = \frac{1}{2}(u_{i,j} + u_{j,i}) \quad i, j = 1, 2.$$

The strains should satisfy the equation of geometrical compatibility

$$(4) \quad \varepsilon_{11,22} + \varepsilon_{22,11} = 2\varepsilon_{12,12}.$$

Let us differentiate the first equation of motion

$$(5) \quad \sigma_{ij,j} = \rho\ddot{u}_i$$

with respect to x_1 , the second with respect to x_2 and then first add them, further subtract these equations. We obtain two equations

$$(6) \quad \sigma_{11,11} + \sigma_{22,22} + 2\sigma_{12,12} = \rho\ddot{e},$$

$$(7) \quad \mathcal{D}_1^2 \sigma_{11} - \mathcal{D}_2^2 \sigma_{22} = \rho(\ddot{\varepsilon}_{11}^0 - \ddot{\varepsilon}_{22}^0),$$

where

$$\mathcal{D}_i^2 = \partial_i^2 - \frac{1}{2c_2^2} \partial_i^2, \quad i = 1, 2, \quad c_2^2 = \frac{\mu}{\rho}.$$

ρ is the density of a body, c_2 is the velocity of the elastic equivoluminal wave.

Let us differentiate the first equation of the system (5) with respect to x_2 , the second with respect to x_1 , then add one to the other. As the result we obtain the equation

$$(8) \quad s_{,12} + \square_2^2 \sigma_{12} = 2\rho \ddot{\varepsilon}_{12}^0,$$

where

$$s = \sigma_{11} + \sigma_{22}, \quad \square_2^2 = \nabla^2 - \frac{1}{c_2^2} \partial_2^2.$$

If we substitute relations (1) in Eq. (6) and make use of Eq. (4), then after some simple calculations we obtain the equation

$$(9) \quad \begin{cases} \square_1^2 s = -2\mu\beta(\varepsilon_{11,22}^0 + \varepsilon_{22,11}^0 - 2\varepsilon_{12,12}^0 - \frac{1}{2c_2^2} \ddot{\varepsilon}_0 + \gamma \square_2^2 \varepsilon_{33}^0), \\ \beta = \frac{2(\lambda + \mu)}{\lambda + 2\mu}, \quad \gamma = \frac{\lambda}{2(\lambda + \mu)}, \quad \varepsilon^0 = \varepsilon_{11}^0 + \varepsilon_{22}^0, \quad \square_1^2 = \nabla^2 - \frac{1}{c_1^2} \partial_1^2, \quad c_2^2 = \frac{\lambda + 2\mu}{\rho}. \end{cases}$$

Eqs. (6), (7) and (9) yield relations between three stress components σ_{11} , σ_{22} , σ_{12} and the components of the distortional field ε_{11}^0 , ε_{12}^0 , ε_{22}^0 , ε_{33}^0 . We introduce three stress functions Φ_i ($i = 1, 2, 3$) connected with the stresses σ_{ij} by the following relations

$$(10) \quad \sigma_{11} = \mathcal{D}_1^2 \Phi_1 + \square_1^2 \Phi_2, \quad \sigma_{22} = \mathcal{D}_2^2 \Phi_1 - \square_1^2 \Phi_2, \quad \sigma_{12} = -\partial_1 \partial_2 \Phi_1 + \square_1^2 \Phi_3.$$

Substituting relations (10) into Eq. (9), (8) and (7), we obtain the system of three equations

$$(11) \quad \square_1^2 \square_2^2 \Phi_i = A_i \quad i = 1, 2, 3,$$

where

$$(12) \quad \begin{cases} A_1 = -2\mu\beta(\varepsilon_{11,22}^0 + \varepsilon_{22,11}^0 - 2\varepsilon_{12,12}^0 - \frac{1}{2c_2^2} \ddot{\varepsilon}_0 + \gamma \square_2^2 \varepsilon_{33}^0), \\ A_2 = \rho(\ddot{\varepsilon}_{11}^0 - \ddot{\varepsilon}_{22}^0), \quad A_3 = 2\rho \ddot{\varepsilon}_{12}^0. \end{cases}$$

From Eq. (11) we determine the particular solutions Φ_i , then by means of relations (10) the stresses σ'_{ij} . The functions Φ'_i do not satisfy all boundary conditions; therefore we add to stresses σ'_{ij} stresses σ''_{ij} expressed by the functions

$$(13) \quad \sigma''_{ij} = -\partial_i \partial_j \varphi + \delta_{ij} \left(\nabla^2 - \frac{1}{2c_2^2} \partial_i^2 \right) \varphi,$$

where the function φ should satisfy the homogeneous equation

$$(14) \quad \square_1^2 \square_2^2 \varphi = 0.$$

According to the T. Boggio theorem [1], Eq. (14) can be replaced by the system of equations

$$(15) \quad \square_1^2 \varphi_1 = 0, \quad \square_2^2 \varphi_2 = 0,$$

where

$$\varphi = \varphi_1 + \varphi_2.$$

The particular solution of Eq. (11) for the infinite elastic space may be given in the form of the Fourier repeated integral [2]

$$(16) \quad \Phi_t(x_1, x_2, t) = \\ = (2\pi)^{-3/2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{\bar{A}_t(a_1, a_2, \omega)}{D(a_1, a_2, \omega)} \exp[-i(a_1 x_1 + a_2 x_2 + \omega t)] da_1 da_2 d\omega,$$

where

$$D(a_1, a_2, \omega) = \left(a_1^2 + a_2^2 - \frac{\omega^2}{c_1^2}\right) \left(a_1^2 + a_2^2 - \frac{\omega^2}{c_2^2}\right)$$

and

$$\bar{A}_1 = 2\mu\beta [(a_2^2 - \kappa\omega^2)\bar{\varepsilon}_{11}^0 + (a_1^2 - \kappa\omega^2)\bar{\varepsilon}_{22}^0 - 2a_1 a_2 \bar{\varepsilon}_{12}^0 + \\ + \gamma(a_1^2 + a_2^2 - 2\kappa\omega^2)\bar{\varepsilon}_{33}^0], \quad \kappa = \frac{1}{2c_2^2},$$

$$\bar{A}_2 = -\rho\omega^2(\bar{\varepsilon}_{11}^0 - \bar{\varepsilon}_{22}^0), \quad \bar{A}_3 = -2\rho\omega^2\bar{\varepsilon}_{12}^0,$$

$$\bar{\varepsilon}_{ij}^0(a_1, a_2, \omega) = (2\pi)^{-3/2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \varepsilon_{ij}^0(x_1, x_2, t) \exp[i(a_1 x_1 + a_2 x_2 + \omega t)] dx_1 dx_2 dt.$$

Let us consider two particular cases of the distortional field ε_{ij}^0 .

a) Let $\varepsilon_{11}^0 = \varepsilon_{22}^0 = \varepsilon_{33}^0 = \eta^0$, $\varepsilon_{12}^0 = 0$. In this case we have $A_2 = A_3 = 0$, and

$$A_1 = -2\mu \frac{3\lambda + 2\mu}{\lambda + 2\mu} \square_2^2 \eta^0.$$

In order to determine the stresses, it is sufficient to take one function Φ satisfying the equation

$$(17) \quad \square_1^2 \square_2^2 \Phi + 2\mu\beta_0 \square_2^2 \eta^0 = 0, \quad \beta_0 = \frac{3\lambda + 2\mu}{\lambda + 2\mu}.$$

The stresses are given by the relations

$$(18) \quad \sigma_{ij} = -\partial_i \partial_j \Phi + \delta_{ij} \left(V^2 - \frac{1}{2c_2^2} \partial_t^2 \right) \Phi, \quad i, j = 1, 2.$$

The solution of Eq. (17) is composed of the particular solution Φ' of the non-homogeneous Eq. (17) and of the general solution Φ'' of the homogeneous Eq. (17), i.e. for $\eta^0 = 0$.

The case here considered contains a thermal distortion, where

$$\varepsilon_{ij}^0 = \alpha_t \delta_{ij} T, \quad i, j = 1, 2, 3.$$

In the infinite space the solution of Eq. (17) is confined only to the particular solution

$$(19) \quad \Phi(x_1, x_2, t) = 2\mu\beta_0 (2\pi)^{-3/2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{\bar{\eta}^0(a_1, a_2, \omega)}{a_1^2 + a_2^2 - \frac{\omega^2}{c_1^2}} \exp[-i(a_1 x_1 + a_2 x_2 + \omega t)] da_1 da_2 d\omega,$$

where

$$\bar{\eta}^0(a_1, a_2, \omega) = (2\pi)^{-3/2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \eta^0(x_1, x_2, t) \exp[i(a_1 x_1 + a_2 x_2 + \omega t)] dx_1 dx_2 dt.$$

If the distortional field varies harmonically in time and p is frequency

$$(20) \quad \eta^0(x_1, x_2, t) = e^{ipt} \eta^*(x_1, x_2).$$

We have also

$$(21) \quad \Phi(x_1, x_2, t) = e^{ipt} \Phi^*(x_1, x_2),$$

and Eq. (17) takes the form

$$(22) \quad (\nabla^2 + k_1^2)(\nabla^2 + k_2^2) \Phi^* + 2\mu\beta_0 (\nabla^2 + k_2^2) \eta^* = 0,$$

where

$$(23) \quad k_i^2 = \frac{p^2}{c_i^2}, \quad i = 1, 2.$$

For the infinite space the following function is the solution of Eq. (22)

$$(24) \quad \Phi^*(x_1, x_2) = 2\mu\beta_0 (2\pi)^{-1} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{\bar{\eta}^*(a_1, a_2)}{a_1^2 + a_2^2 - k_1^2} \exp[-i(a_1 x_1 + a_2 x_2)] da_1 da_2,$$

where

$$\bar{\eta}^*(a_1, a_2) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \eta^*(x_1, x_2) \exp[i(a_1 x_1 + a_2 x_2)] dx_1 dx_2.$$

If the distortional field $\eta^0(x_1, x_2, t)$ moves in the x_1 -axis direction with constant velocity c , then transforming the co-ordinates

$$(25) \quad \xi_1 = x_1 - ct, \quad \xi_2 = x_2,$$

we reduce Eq. (17) to the form

$$(26) \quad (\partial_1^2 + \gamma_1^2 \partial_2^2)(\partial_1^2 + \gamma_2^2 \partial_2^2) \Phi(\xi_1, \xi_2) + 2\mu\beta_0 \gamma_1^2 (\partial_1^2 + \gamma_2^2 \partial_2^2) \eta^0(\xi_1, \xi_2) = 0,$$

where

$$\gamma_i^2 = \left(1 - \frac{c^2}{c_i^2}\right)^{-1}, \quad \partial_i = \frac{\partial}{\partial \xi_i}, \quad i = 1, 2.$$

The solution of Eq. (26) for the infinite space is given by the integral

$$(27) \quad \Phi(\xi_1, \xi_2) = \frac{\mu\beta_0 \gamma_1^2}{\pi} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{\bar{\eta}^0(a_1, a_2)}{a_1^2 + a_2^2 \gamma_1^2} \exp[-i(a_1 \xi_1 + a_2 \xi_2)] da_1 da_2,$$

where

$$\bar{\eta}^0(a_1, a_2) = (2\pi)^{-1} \int_{-\infty}^{\infty} \eta^0(\xi_1, \xi_2) \exp[i(a_1 \xi_1 + a_2 \xi_2)] d\xi_1 d\xi_2.$$

Observe that the distortional field $\eta^0(x_1, x_2, t)$ produces in the infinite space only longitudinal waves.

b) Let $\varepsilon_{11}^0 = \varepsilon_{22}^0 = \varepsilon_{33}^0 = 0$, $\varepsilon_{12}^0 = \vartheta^0$. In this case we have

$$(28) \quad A_1 = 4\mu\beta \vartheta_{,12}^0, \quad A_2 = 0, \quad A_3 = 2\rho \vartheta_{,12}^0.$$

In order to determine the state of stresses, it is sufficient to take two functions satisfying the equations

$$(29) \quad \square_1^2 \square_2^2 \Phi_1 = A_1, \quad \square_1^2 \square_2^2 \Phi_3 = A_3.$$

The stresses are given by the relations

$$(30) \quad \sigma_{11} = \mathcal{D}_2^2 \Phi_1, \quad \sigma_{22} = \mathcal{D}_1^2 \Phi_1, \quad \sigma_{12} = -\partial_1 \partial_2 \Phi_1 + \square_1^2 \Phi_3.$$

In the infinite space the solutions of Eq. (29) are given by Fourier's integrals (16), for $i = 1, 2, 3$, where

$$(31) \quad \bar{A}_1 = -4\mu\beta a_1 a_2 \bar{\vartheta}^0, \quad \bar{A}_2 = 0, \quad \bar{A}_3 = 2\rho \omega^2 a_1 a_2 \bar{\vartheta}^0.$$

If the distortional field varies slowly in time, then in Eqs. (6), (7) and (9), we can neglect the inertial terms. The system of equations

$$(32) \quad \begin{cases} \nabla^2 s = -2\mu\beta (\varepsilon_{11,22}^0 + \varepsilon_{22,11}^0 - 2\varepsilon_{12,12}^0 + \gamma \nabla^2 \varepsilon_{33}^0), \\ \partial_1^2 \sigma_{11} - \partial_2^2 \sigma_{22} = 0, \quad s_{,12} + \nabla^2 \sigma_{12} = 0, \end{cases}$$

is satisfied by function F ; moreover, [3]

$$(33) \quad \nabla^2 \nabla^2 F = -2\mu\beta (\varepsilon_{11,22}^0 + \varepsilon_{22,11}^0 - 2\varepsilon_{12,12}^0 + \gamma \nabla^2 \varepsilon_{33}^0),$$

and

$$(34) \quad \sigma_{ij} = -(\partial_i \partial_j - \delta_{ij} \nabla^2) F.$$

The solution of Eq. (33) can be represented in the form

$$(35) \quad F = -2\mu\beta \int \int_{(\gamma)} \left(\varepsilon_{11}^0 \frac{\partial^2 F^*}{\partial \xi_2^2} + \varepsilon_{22}^0 \frac{\partial^2 F^*}{\partial \xi_1^2} - 2\varepsilon_{12}^0 \frac{\partial^2 F^*}{\partial \xi_1 \partial \xi_2} + \gamma \varepsilon_{33}^0 \nabla_{\xi_1, \xi_2}^2 F^* \right) d\xi_1 d\xi_2,$$

where F^* is the Green function satisfying the equation

$$(36) \quad \nabla^2 \nabla^2 F^* = \delta(x_1 - \xi_1) \delta(x_2 - \xi_2).$$

If the boundary of the infinite cylinder (the axis parallel to x_3) is free from stresses on the curved surface ($F = F_{,n} = 0$, $F^* = F^*_{,n} = 0$), then solution (35) can be represented in the form [4]

$$(37) \quad F = -2\mu\beta \int \int_{(r)} F^* \left(\frac{\partial^2 \varepsilon_{11}^0}{\partial \xi_2^2} + \frac{\partial^2 \varepsilon_{22}^0}{\partial \xi_1^2} - 2 \frac{\partial^2 \varepsilon_{12}^0}{\partial \xi_1 \partial \xi_2} + \gamma V^2 \varepsilon_{33}^0 \right) d\xi_1 d\xi_2.$$

In the particular case of the steady temperature field in the absence of heat sources ($\varepsilon_{ij}^0 = \delta_{ij} \alpha_l T$, $\nabla^2 T = 0$) we have $F = 0$ at each point of the cylinder. Thus we have only one component of the stresses σ_{33} .

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