

The State of Stress in an Elastic Space Due to a Source of Heat Varying Harmonically in Function of Time

by

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Let a concentrated source of heat of intensity variable in a harmonic manner act at the point A constituting the origin of the co-ordinate system. The action of this source will result in a time-variable temperature and stress field T and σ_{ij} , respectively, both varying also in a harmonic manner. Assume that the frequency of vibration of the heat source is insignificant, so that the phenomenon under consideration can be treated as quasi-static. The acceleration containing terms in displacement equations of the theory of elasticity will therefore be dropped.

The temperature field is determined by the equation

$$(1.1) \quad \nabla^2 T = \frac{1}{k} \frac{\partial T}{\partial t} - \frac{W}{\lambda} \delta(x) \delta(y) \delta(z),$$

where $k = \lambda/\rho c$, λ is the coefficient of heat conduction, ρ — density and c — specific heat. The symbol δ denotes the Dirac function.

In view of the harmonic character of the action of the source, we assume

$$(1.2) \quad T(x, y, z, t) = U(x, y, z) e^{i(\omega t - t)}, \quad W = W_0 e^{i(\omega t - t)}.$$

The Eq. (1.1) may therefore be reduced to the form

$$(1.3) \quad \nabla^2 U - i\eta U = -\frac{W_0}{\lambda} \delta(x) \delta(y) \delta(z) \quad \eta = \frac{\omega}{k}.$$

The solution of this equation in cylindrical co-ordinates, assuming $T = 0$ at infinity, is

$$(1.4) \quad U = \frac{W}{2\pi^2\lambda} \int_0^\infty \int_0^\infty a(a^2 + \gamma^2 + i\eta)^{-1} J_0(ar) \cos \gamma z da d\gamma, \quad r = (x^2 + y^2)^{1/2}.$$

After integration, we have

$$(1.5) \quad U = \frac{W_0}{4\pi\lambda} R^{-1} \exp(-R\sqrt{i\eta}), \quad R = (x^2 + y^2 + z^2)^{1/2}.$$

Bearing in mind (1.2), we find that

$$(1.6) \quad T = \frac{W_0}{4\pi\lambda} R^{-1} \exp[i(\omega t - \varepsilon) - R\sqrt{i\eta}].$$

The temperature field T will be obtained as the real part of the expression (1.6):*

$$(1.7) \quad T = \frac{W_0}{4\pi\lambda} R^{-1} \exp\left(-R\sqrt{\frac{\omega}{2k}}\right) \cdot \cos\left(\omega t - \varepsilon - R\sqrt{\frac{\omega}{2k}}\right).$$

It will be convenient for the determination of stress to use the potential of thermo-elastic stress Φ .

This function is related to the temperature field.

Thus, [1], we have

$$(1.8) \quad \nabla^2 \Phi = \frac{1+\nu}{1-\nu} \alpha_t T,$$

where ν is Poisson's ratio and α_t — the coefficient of thermal dilatation. In view of the harmonic character of the source, we assume that

$$(1.9) \quad \Phi(x, y, z, t) = \operatorname{Re} \{ \Psi(x, y, z) e^{i(\omega t - \varepsilon)} \}.$$

Thus,

$$(1.10) \quad \nabla^2 \Psi = \frac{1+\nu}{1-\nu} \alpha_t U.$$

Bearing in mind the Eq. (1.4), the solution of the above equation has the form

$$(1.11) \quad \Psi = -\frac{W_0 \alpha_t}{2\pi^2 \lambda} \frac{1+\nu}{1-\nu} \int_0^\infty \int_0^\infty a (a^2 + \gamma^2)^{-1} (a^2 + \gamma^2 + i\eta)^{-1} \times \\ \times J_0(ar) \cos \gamma z \, da \, d\gamma,$$

or, after integration,

$$(1.12) \quad \Psi = \frac{1+\nu}{1-\nu} \frac{\alpha_t W_0}{4\pi\lambda\eta} i [1 - \exp(-R\sqrt{i\eta})] R^{-1}.$$

The real part of the function Φ in the Eq. (1.9) will take the form

$$(1.13) \quad \Phi = -\frac{1+\nu}{1-\nu} \alpha_t \frac{W_0 k}{4\pi\lambda\omega} R^{-1} \left\{ \sin \left[R\sqrt{\frac{\omega}{2k}} - \omega t + \varepsilon \right] \times \right. \\ \left. \times \exp \left(-R\sqrt{\frac{\omega}{2k}} \right) + \sin(\omega t - \varepsilon) \right\}.$$

* We assume here that $W(t) = W_0 \cos(\omega t - \varepsilon)$.

Knowing the function ϕ , we are able to determine the stress components from

$$(1.14) \quad \sigma_{ij} = 2G \left(\frac{\partial^2 \phi}{\partial i \partial j} - V^2 \phi \delta_{ij} \right), \quad i, j = x, y, z,$$

where δ_{ij} is Kronecker's delta.

We are concerned in our problem with a symmetry of the spherical type. In spherical co-ordinates we obtain the most simple expression for stress components. We have

$$(1.15) \quad \sigma_{rr} = 2G \left(\frac{d^2 \phi}{dR^2} - V^2 \phi \right), \quad \sigma_{\varphi\varphi} = \sigma_{\vartheta\vartheta} = 2G \left(\frac{1}{R} \frac{d\phi}{dR} - V^2 \phi \right),$$

$$\sigma_{r\varphi} = 0, \quad \sigma_{r\vartheta} = 0, \quad \sigma_{\varphi\vartheta} = 0, \quad V^2 \phi = \frac{d^2 \phi}{dR^2} + \frac{2}{R} \frac{d\phi}{dR}.$$

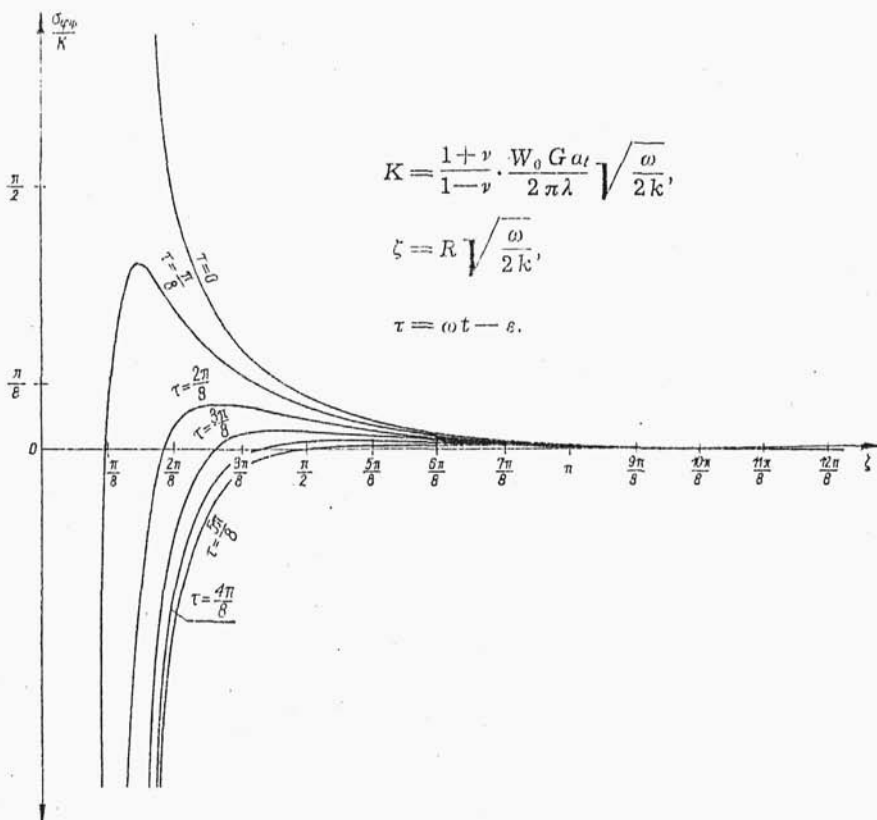


Fig. 1a

Using the Eq. (1.13), we find that

$$\sigma_{rr} = \frac{(1+\nu) \alpha_l k W_0 G}{(1-\nu) \pi \lambda \omega} \left\{ \exp \left(-R \sqrt{\frac{\omega}{2k}} \right) \left[\left(1 + R \sqrt{\frac{\omega}{2k}} \right) \times \right. \right. \\ \left. \left. \times \sin \left(\omega t - \varepsilon - R \sqrt{\frac{\omega}{2k}} \right) + R \sqrt{\frac{\omega}{2k}} \right] - \sin (\omega t - \varepsilon) \right\} R^{-3}, \quad (1.16)$$

$$\sigma_{\varphi\varphi} = \sigma_{\vartheta\vartheta} = -\sigma_{rr} - \frac{(1+\nu) \alpha_l W_0 G k}{(1-\nu) 2 \lambda \pi \omega} R^{-1} \exp \left(-R \sqrt{\frac{\omega}{2k}} \right) \times \\ \times \cos \left(\omega t - \varepsilon - R \sqrt{\frac{\omega}{2k}} \right) = -\sigma_{rr} - \frac{1+\nu}{1-\nu} \alpha_l 2 G T, \quad \sigma_{qr} = \sigma_{r\vartheta} = \sigma_{\vartheta r} = 0.$$

In Fig. 1a the diagram of the function $\sigma_{\varphi\varphi}$ is given. Fig. 1b represents that of σ_{rr} for a few values of the parameters $\tau = \omega t - \varepsilon$.

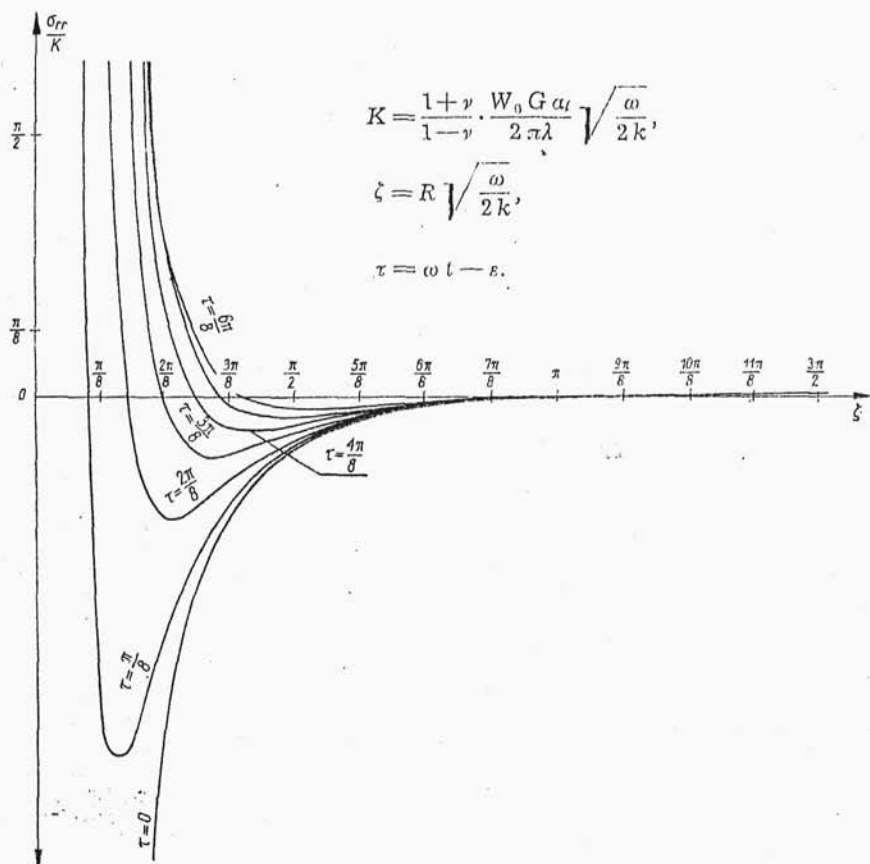


Fig. 1b

Let heat sources uniformly distributed along the z -axis, act in the elastic space. The problem is axially symmetric. The heat equation takes the form

$$(1.17) \quad \frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} = \frac{1}{k} \frac{\partial T}{\partial t} - \frac{W}{\lambda} \delta(r).$$

For a linear source of intensity W per unit length we assume that it changes with time in a harmonic manner, and

$$(1.18) \quad T(r, t) = U(r) e^{i(\omega t - \varepsilon)}, \quad W = W_0 e^{i(\omega t - \varepsilon)}.$$

The Eq. (1.17) takes the form

$$(1.19) \quad \frac{d^2 U}{dr^2} + \frac{1}{r} \frac{dU}{dr} - i\eta U = -\frac{W_0}{\lambda} \delta(r).$$

The solution of the Eq. (1.19) is the integral

$$(1.20) \quad U = \frac{W_0}{2\pi\lambda} \int_0^\infty a J_0(ar) (a^2 + i\eta)^{-1} da = \frac{W_0}{2\pi\lambda} K_0(r\sqrt{i\eta}),$$

where $K_0(r\sqrt{i\eta})$ is a modified Bessel function of the third kind otherwise called a Basset function. Thus,*)

$$(1.21) \quad T = Re \left[\frac{W_0}{2\pi\lambda} e^{i(\omega t - \varepsilon)} K_0(r\sqrt{i\eta}) \right].$$

Bearing in mind that

$$e^{-\frac{i\nu\pi}{2}} K_0(r\sqrt{i\eta}) = \ker_\nu(r\sqrt{\eta}) + i \operatorname{kei}_\nu(r\sqrt{\eta}),$$

where the functions $\ker_\nu(z)$, $\operatorname{kei}_\nu(z)$ are Kelvin functions, we can express the real part of the function (1.21) by

$$(1.22) \quad T = \frac{W_0}{2\pi\lambda} \left[\ker_0 \left(r \sqrt{\frac{\omega}{2k}} \right) \cos(\omega t - \varepsilon) - \operatorname{kei}_0 \left(r \sqrt{\frac{\omega}{2k}} \right) \sin(\omega t - \varepsilon) \right].$$

From the equation

$$\frac{\partial^2 \Phi}{\partial r^2} + \frac{1}{r} \frac{\partial \Phi}{\partial r} = \frac{1+\nu}{1-\nu} \alpha_t T$$

we determine the function Φ in the form

$$(1.23) \quad \begin{aligned} \Phi &= -Re \left[\frac{W_0}{2\pi\lambda} \int_0^\infty a^{-1} (a^2 + i\eta)^{-1} J_0(a, r) da \right] = \\ &= \frac{1+\nu}{1-\nu} \frac{W_0}{2\pi\lambda} \frac{\alpha_t}{i\eta} \left[\ln \frac{a}{r} - K_0(r\sqrt{i\eta}) \right]. \end{aligned}$$

* For $W = W_0 \cos(\omega t - \varepsilon)$.

Knowing the function ϕ , we can determine the complex stress from the following equation:

$$(1.24) \quad \sigma_{rr}^* = -2G \frac{1}{r} \frac{\partial \phi}{\partial r}, \quad \sigma_{\theta\theta}^* = -2G \frac{\partial^2 \phi}{\partial r^2}, \quad \sigma_{r\theta}^* = 0.$$

We obtain

$$(1.25) \quad \begin{cases} \sigma_{rr}^* = \frac{1+\nu}{1-\nu} \alpha_t \frac{W_0 G}{\pi \lambda} \frac{e^{i(\omega t - \varepsilon)}}{i\eta} \left[\sqrt{i\eta} K_1(r\sqrt{i\eta}) - \frac{1}{r^2} \right], \\ \sigma_{\theta\theta}^* = -\frac{1+\nu}{1-\nu} \alpha_t \frac{W_0 G}{\pi \lambda} \frac{e^{i(\omega t - \varepsilon)}}{i\eta} \left[\sqrt{i\eta} K_1(r\sqrt{i\eta}) + \eta i K_0(r\sqrt{i\eta}) - \frac{1}{r^2} \right] = \\ \sigma_{r\theta}^* = 0. \end{cases} = -\sigma_{rr}^* - \frac{1+\nu}{1-\nu} \alpha_t 2GT,$$

The stresses σ_{rr} , $\sigma_{\theta\theta}$ will be obtained as the real parts of the functions σ_{rr}^* , $\sigma_{\theta\theta}^*$.

We have

$$(1.26) \quad \begin{aligned} \sigma_{rr} = & -\frac{1+\nu}{1-\nu} \alpha_t \frac{W_0 G k}{\pi \lambda \omega} \left\{ \sqrt{\frac{\omega}{2k}} \left[\operatorname{kei}_1 \left(r \sqrt{\frac{\omega}{2k}} \right) - \right. \right. \\ & \left. \left. - \operatorname{ker}_1 \left(r \sqrt{\frac{\omega}{2k}} \right) \right] \cos(\omega t - \varepsilon) + \left[\operatorname{ker}_1 \left(r \sqrt{\frac{\omega}{2k}} \right) + \right. \right. \\ & \left. \left. + \operatorname{kei}_1 \left(r \sqrt{\frac{\omega}{2k}} \right) \right] \sin(\omega t - \varepsilon) \right\} + \frac{1}{r^3} \sin(\omega t - \varepsilon) \Big\}, \\ \sigma_{\theta\theta} = & -\sigma_{rr} - \frac{1+\nu}{1-\nu} \alpha_t \frac{W_0 G}{\pi \lambda} \left[\operatorname{ker}_0 \left(r \sqrt{\frac{\omega}{2k}} \right) \cos(\omega t - \varepsilon) - \operatorname{kei}_0 \times \right. \\ & \left. \times \left(r \sqrt{\frac{\omega}{2k}} \right) \sin(\omega t - \varepsilon) \right]. \end{aligned}$$

Let us now consider the following problem. Let uniformly distributed heat sources act in the plane $x = \xi$ of an elastic space. The intensity of these stresses per unit area of the plane $x = \xi$ will be denoted by $W = W_0 e^{i(\omega t - \varepsilon)}$.

The heat equation is

$$(1.27) \quad \frac{\partial^2 T}{\partial x^2} = \frac{1}{k} \frac{\partial T}{\partial t} - \frac{W}{\lambda} \delta(x - \xi).$$

Introducing the relation $T(x, t) = U(x) e^{i(\omega t - \varepsilon)}$, we reduce the partial differential equation (1.27) to the ordinary equation

$$(1.28) \quad \frac{d^2 U}{dx^2} - i\eta U = -\frac{W_0}{\lambda} \delta(x - \xi).$$

The solution of this equation is

$$(1.29) \quad U = \frac{W_0}{\lambda \pi} \int_0^{\infty} (a^2 + i\eta)^{-1} \cos a(x - \xi) da = \\ = \frac{W_0}{2\lambda} (i\eta)^{-1/2} \exp[-(x - \xi) \sqrt{i\eta}].$$

Hence,

$$(1.30) \quad T = Re \left\{ \frac{W_0}{2\lambda} (i\eta)^{-1/2} \exp[i(\omega t - \varepsilon) - (x - \xi) \sqrt{i\eta}] \right\}.$$

The real part of this function is the temperature field

$$(1.31) \quad T = \frac{W_0}{4\lambda} (\eta)^{-1/2} \exp[-(x - \xi) \sqrt{\eta}] \cos[\omega t - \varepsilon - (x - \xi) \sqrt{\eta}]$$

which is sought.

The Eq. (1.8) reduces to the form

$$(1.32) \quad \frac{\partial^2 \phi}{\partial x^2} = \frac{1+\nu}{1-\nu} a_t T.$$

From (1.14) it is seen that

$$\sigma_{xx} = 0, \quad \sigma_{zx} = 0, \quad \sigma_{zy} = 0, \quad \sigma_{xy} = 0,$$

and

$$(1.33) \quad \sigma_{yy} = \sigma_{zz} = -2G \frac{\partial^2 \phi}{\partial x^2} = -2G \frac{1+\nu}{1-\nu} a_t T.$$

Thus,

$$(1.34) \quad \sigma_{yy} = \sigma_{zz} = \frac{G W_0 a_t (1+\nu)}{2\lambda (1-\nu)} \left(\frac{2k}{\omega} \right)^{1/2} \exp \left[-(x - \xi) \sqrt{\frac{\omega}{2k}} \right] \times \\ \times \cos \left[\omega t - \varepsilon - (x - \xi) \sqrt{\frac{\omega}{2k}} \right].$$

In Figure 2 the function σ_{yy} is represented for various values of the parameters $\tau = \omega t - \varepsilon$.

Let a positive plane heat source act in the plane $x = \xi$ and a negative plane source in the plane $x = -\xi$. In this case we have $T = 0$ and $\sigma_{yy} = 0$, $\sigma_{xx} = 0$ in the plane $x = 0$.

We are concerned with the case of an elastic semi-space ($x > 0$) in which a plane heat source acts in the plane $x = \xi$.

The stresses σ_{yy} , σ_{zz} will be obtained from the equations

$$(1.35) \quad \sigma_{yy} = \sigma_{zz} = \frac{G W_0 a_t (1+\nu)}{2\lambda (1-\nu)} \left(\frac{2k}{\omega} \right)^{1/2} \left\{ \exp \left[-(x - \xi) \sqrt{\frac{\omega}{2k}} \right] \times \right. \\ \times \cos \left[\omega t - \varepsilon - (x - \xi) \sqrt{\frac{\omega}{2k}} \right] - \exp \left[-(x + \xi) \sqrt{\frac{\omega}{2k}} \right] \times \\ \left. \times \cos \left[\omega t - \varepsilon - (x + \xi) \sqrt{\frac{\omega}{2k}} \right] \right\} \quad \text{for } x > \xi.$$

For $x < \xi$ we should replace $(x - \xi)$ by $(\xi - x)$.

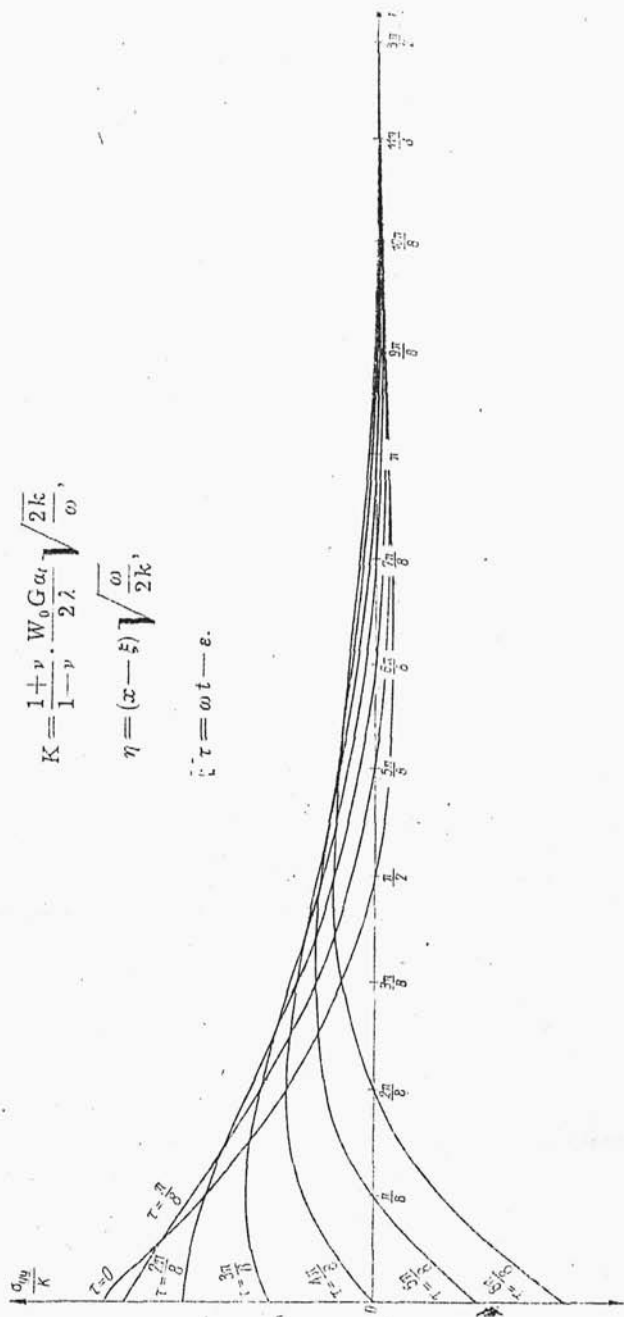


Fig. 2

$$K = \frac{1+\nu}{1-\nu} \cdot \frac{W_0 G_{01}}{2\lambda} \sqrt{\frac{2k}{\omega}},$$

$$\eta = x \sqrt{\frac{\omega}{2k}},$$

$$\xi \sqrt{\frac{\omega}{2k}} = \frac{\pi}{2},$$

$$\tau = \omega t - \varepsilon.$$

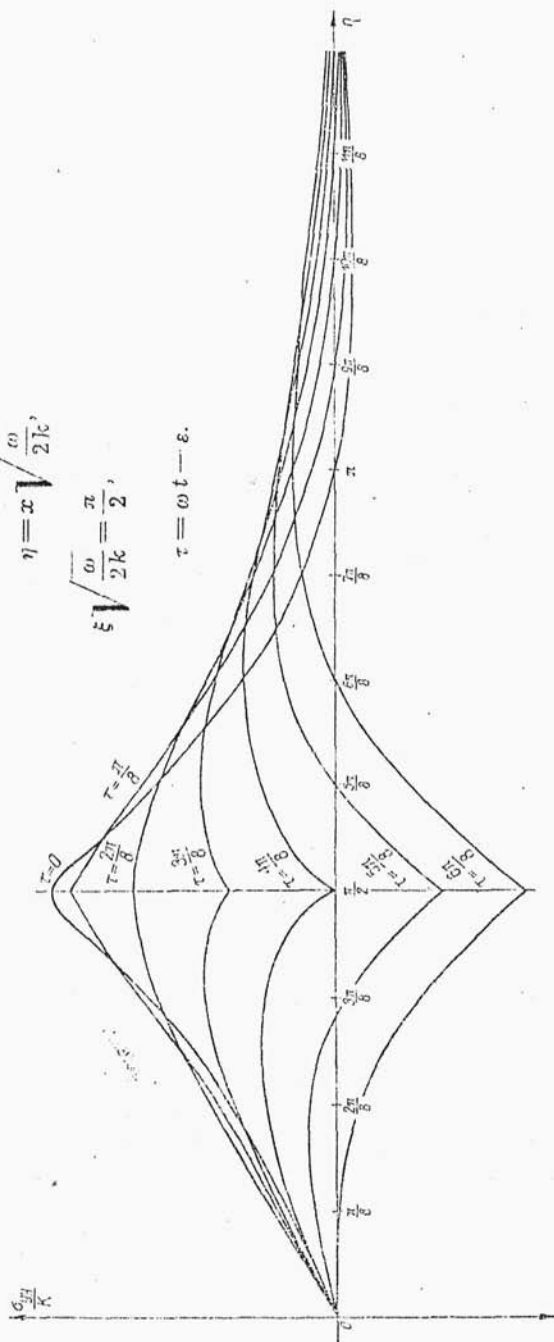


Fig. 3.



In Figure 3 the function σ_{yy} is represented for various values of the parameter τ .

The solutions obtained for a heat source varying in a harmonic manner can be used for constructing solutions changing in a periodic manner.

Expanding the function $W(t)$ in a Fourier series

$$(1.36) \quad W(t) = \sum_{n=0}^{\infty} A_n \cos(n\omega t - \epsilon_n),$$

we obtain the temperature and stress field as a result of superposition of harmonic elements.

Thus, in the case of a source of intensity $W(t)$ acting in an infinite elastic space and varying with time in a periodic manner, we obtain for the temperature field the following expression:

$$(1.37) \quad T = \frac{1}{4\pi\lambda R} \sum_{n=0}^{\infty} A_n \exp\left(-R\sqrt{\frac{\omega n}{2k}}\right) \cos\left(n\omega t - \epsilon_n - R\sqrt{\frac{\omega n}{2k}}\right).$$

Moreover, the solutions obtained can be used to determine the temperature and stress fields in the case of heat sources distributed over any region I' of the elastic space. If in the region I' there acts a heat source, constituting a harmonic function of time and any function of the co-ordinate, the temperature field will be expressed as

$$T(x, y, z, t) = \frac{1}{4\pi\lambda} \int_{(I')} \int \frac{W_0(\xi, \eta, \zeta)}{R} \exp\left(-R\sqrt{\frac{\omega}{2k}}\right) \times \\ \times \cos\left(\omega t - \epsilon - R\sqrt{\frac{\omega}{2k}}\right) d\xi d\eta d\zeta,$$

where

$$R = [(x - \xi)^2 + (y - \eta)^2 + (z - \zeta)^2]^{1/2}.$$

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