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## Thermal Stresses in Elastic and Viscoelastic Shells

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The purpose of the present paper is to determine the displacements produced in shells by a field of initial deformations (distortions), in particular by the field of temperature. The starting point for our considerations is the reciprocal theorem for a three-dimensional elastic body, distortions being taken into account. This theorem will be specialized to the plane state of stresses in shells. The theorem in three-dimensional state of stresses assumes the form [1], [2]:

$$(1.1) \quad \int_V X'_i u''_i dV + \int_S p'_i u''_i dS + \int_V \varepsilon_{ij}^{0'} \sigma'_{ij} dV = \int_V X''_i u'_i dV + \int_S p''_i u'_i dS + \\ + \int_V \varepsilon_{ij}^{0''} \sigma'_{ij} dV, \\ i, j = 1, 2, 3.$$

In the above equation there appear two states denoted correspondingly by "prime" and "double prime". Thus, in the first state  $u'_i$  denote the components of displacement vector  $\vec{u}'$ ;  $X'_i$  are the components of the body forces vector  $\vec{X}'$ , while  $p'_i$  are the components of the vector of surface loadings  $\vec{p}'$ ;  $\sigma'_{ij}$  denote the stress tensor components and  $\varepsilon_{ij}^{0'}$  are the distortion components.  $\lambda$  and  $\mu$  are the Lamé constants. The integration is performed over volume  $V$  and surface  $S$  bounding an elastic body.

Let us consider an elastic body clamped on the part  $S_1$  of the region  $S$  and on the remaining part  $S_2$  free from loadings. Suppose the required displacements  $u'_i$  to be produced by distortions  $\varepsilon_{ij}^{0'}$ . We assume that  $X'_i = 0$ . As the second state of loading we assume the concentrated unit force acting at point  $(\xi)$  and directed along the  $x_k$  axis. Moreover, let  $\varepsilon_{ij}^{0''} = 0$ . Substituting in (1.1)  $X'_i = 0$ ,  $\varepsilon_{ij}^{0''} = 0$ , and

$$X''_i = \delta(x_1 - \xi_1) \delta(x_2 - \xi_2) \delta(x_3 - \xi_3) \delta_{ik},$$

and taking into account that the surface integrals vanish, we obtain:

$$(1.2) \quad 1''_k u'_k(\xi) = \int [2\mu \varepsilon_{ij}^{0'}(x) \varepsilon''_{ij}{}^{(k)}(x, \xi) + \lambda e^{0'}(x) e''{}^{(k)}(x, \xi)] dV(x), \\ i, j, k = 1, 2, 3.$$

Deformations  $\varepsilon''_{ij}{}^{(k)}(x, \xi)$  and dilatation  $e''{}^{(k)}(x, \xi)$  are Green functions; they denote the deformations and the dilatation at point  $(x)$  produced by the action of

the concentrated force applied at  $(\xi)$  and directed along the  $x_k$  axis. Eq. (1.2) may be written also in the following form:

$$(1.3) \quad u'_k(\xi) = \int_V \varepsilon_{ij}^0(x) \sigma''_{ij}{}^{(k)}(x, \xi) dV(x), \quad i, j, k = 1, 2, 3,$$

where the components of the stress state produced by the action of the concentrated force at point  $(\xi)$  and directed along the  $x_k$  axis are denoted by  $\sigma''_{ij}{}^{(k)}(x, \xi)$ . The stresses  $\sigma''_{ij}{}^{(k)}$  are given by the formulae

$$(1.4) \quad \begin{aligned} \sigma''_{ij}{}^{(k)} &= 2\mu(\gamma_{ij}^{(k)} + x_3 \varkappa_{ij}^{(k)}) + \eta \delta_{ij}(\gamma^{(k)} + x_3 \varkappa^{(k)}), \\ \gamma^{(k)} &= \gamma_{jj}^{(k)}, \quad \varkappa^{(k)} = \varkappa_{jj}^{(k)}, \quad \eta = \frac{2\mu\lambda}{\lambda + 2\mu}. \end{aligned}$$

Suppose that distortions  $\varepsilon_{ij}^0$  are linear functions of  $x_3$

$$(1.5) \quad \varepsilon_{ij}^0 = \psi_{ij}^0 + x_3 \varphi_{ij}^0, \quad \psi_{ij}^0 \equiv \psi_{ij}^0(x_1, x_2), \quad \varphi_{ij}^0 \equiv \varphi_{ij}^0(x_1, x_2).$$

If we substitute (1.5) into (1.3) and make use of relations (1.4), then performing the integration with respect to  $x_3$ , we obtain the following formulae for displacement:

$$(1.6) \quad u_k(\xi_1, \xi_2) = \int \int_{(r)} [\psi_{ij}^0(x_1, x_2) N_{ij}^{(k)}(x_1, x_2, \xi_1, \xi_2) + \varphi_{ij}^0(x_1, x_2) M_{ij}^{(k)}(x_1, x_2, \xi_1, \xi_2)] dx_1, dx_2$$

Here,  $N_{ij}^{(k)}$  denote the normal and shear forces,  $M_{ij}^{(k)}$  — the bending moments and torques produced in the shell by the action of the concentrated force at point  $(\xi)$  and directed along the  $x_k$  axis.

This method of solution briefly outlined above may be extended on the problems of shells and even — making use of the elastic-viscoelastic analogy — on the viscoelastic shells.

In the final part an example is given relating to the thermal stresses in an open cylindrical shell.

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