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## The Plane Non-coupled Dynamic Problem of Thermoelasticity

by

W. NOWACKI

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### 1. General equations

In Ref. [1] it has been shown that the plane non-coupled dynamic problem of thermoelasticity (for plane strain) can be treated in stresses by means of the stress function  $F$  connected with the stresses by the relations

$$(1.1) \quad \sigma_{ij} = -F_{,ij} + \delta_{ij} \left( F_{,kk} - \frac{1}{2c_2^2} \ddot{F} \right), \quad i, j = 1, 2,$$

and satisfying the non-homogeneous bi-wave equation

$$(1.2) \quad \square_1^2 \square_2^2 F + 2\mu m \square_2^2 T = 0,$$

where  $T$  is the temperature,  $\mu\lambda$  — the Lamé constants,  $a_t$  — the coefficient of thermal dilatation and  $m = \frac{(3\lambda+2\mu)a_t}{\lambda+2\mu}$ ,  $\square_1^2, \square_2^2$  are the differential operators

$$(1.3) \quad \square_1^2 = \nabla^2 - \frac{1}{c_1^2} \partial_t^2, \quad \square_2^2 = \nabla^2 - \frac{1}{c_2^2} \partial_t^2,$$

where  $\nabla^2$  is the Laplacian operator and  $c_1$  and  $c_2$  are the velocities of propagation of the longitudinal and transversal elastic waves, respectively,

$$c_1^2 = \frac{\lambda+2\mu}{\varrho}, \quad c_2 = \frac{\mu}{\varrho}.$$

The other symbols are  $\delta_{ij}$  — Kronecker's delta,  $\varrho$  — density and  $\partial_t$  — the symbol of time derivative.

The temperature  $T$  should satisfy the heat equation

$$(1.4) \quad \square_3^2 T = -\frac{Q}{\kappa}, \quad \square_3^2 = \nabla^2 - \frac{1}{\kappa} \partial_t,$$

where  $\kappa = \frac{\lambda'}{c\varrho}$ ,  $Q = \frac{W}{c\varrho}$  and  $\lambda'$  is the coefficient of heat conduction,  $W$  — the quantity of heat produced per unit volume and time and  $c$  — the specific heat.

The solution of the Eq. (1.1) may be expressed in the form of a sum of three functions  $F = F_0 + F^*$ ,  $F^* = F_1 + F_2$ , where  $F_0$  is a particular integral of (1.2), and  $F_1$ ,  $F_2$  are the general integrals satisfying the equation

$$(1.5) \quad \square_1^2 F_1 = 0, \quad \square_2^2 F_2 = 0.$$

In the case of the infinite space it suffices to determine a particular integral of the equation

$$(1.6) \quad \square_1^2 F_0 + 2\mu m T = 0.$$

For a limited body, in addition to the particular integral  $F_0$  the functions  $F_1$  and  $F_2$  should be determined. The particular integral  $F_0$  should be selected in such a way that some of the conditions of the problem will be satisfied. The determination of the particular integral may be done in the following way.

Let us eliminate the temperature from the equations (1.4) and (1.6). Then,

$$(1.7) \quad \square_1^2 \square_3^2 F_0 = \frac{2\mu m}{\kappa} Q.$$

Bearing in mind that

$$(1.8) \quad \square_1^2 \square_3^2 = \frac{\square_1^2 - \square_3^2}{(\square_3^2)^{-1} - (\square_1^2)^{-1}}, \quad \square_1^2 - \square_3^2 = \frac{1}{\kappa} \partial_t - \frac{1}{c_1^2} \partial_t^2,$$

Eq. (1.7) may be represented in the form:

$$(1.9) \quad \left( \frac{1}{\kappa} \partial_t - \frac{1}{c_1^2} \partial_t^2 \right) F_0 = -\frac{2\mu m}{\kappa} [(\square_3^2)^{-1} - (\square_1^2)^{-1}] Q.$$

Let us introduce an auxiliary function  $S$ , satisfying the equation

$$(1.10) \quad \square_1^2 S = -Q/\kappa,$$

and assume that function  $S$  satisfies the same boundary conditions as function  $T$ . Since

$$(1.11) \quad T = -\frac{1}{\kappa} (\square_3^2)^{-1} Q, \quad S = -\frac{1}{\kappa} (\square_1^2)^{-1} Q,$$

Eq. (1.9) takes the form

$$(1.12) \quad \left( \frac{1}{\kappa} \partial_t - \frac{1}{c_1^2} \partial_t^2 \right) F_0 = 2\mu m (T - S).$$

A number of particular solutions can be obtained in a simple way from (1.12).

Let us assume that the action of the heat sources started at  $t > 0$  and for  $t \leq 0$  the body was in the natural, undeformed and unstressed state. On performing the Laplace transformation on Eq. (1.12), we obtain

$$(1.13) \quad \tilde{F}_0 = \frac{2\mu m}{(p/\kappa - p^2/c_1^2)} (\tilde{T} - \tilde{S}),$$

where

$$\tilde{F}_0(x_r, p) = \int_0^\infty (x_r, t) e^{-pt} dt, \text{ etc.}$$

The inverse Laplace transformation yields the function  $F_0$ , and the Eqs. (1.1) — the stresses corresponding to this function.

If the heat sources are harmonic in time  $Q(x_r, t) = e^{i\omega t} Q_0(x_r)$  the functions  $T, F_0, S$  are also harmonic.

Inserting

$$T(x_r, t) = e^{i\omega t} U(x_r), \quad S(x_r, t) = e^{i\omega t} V(x_r), \quad F_0(x_r, t) = e^{i\omega t} \Phi_0(x_r),$$

into (1.12),  $\Phi_0$  is obtained from the equation

$$(1.14) \quad \Phi_0 = \frac{2\mu m (U - V)}{i\eta + k^2}, \quad \eta = \omega/\kappa, \quad k^2 = \omega^2/c_1^2.$$

The stresses corresponding to the function  $F_0$  are expressed by

$$(1.15) \quad \sigma_{ij} = e^{i\omega t} \left[ \Phi_0, ij + \delta_{ij} \left( V^2 + \frac{\omega^2}{2c_2^2} \right) \Phi_0 \right], \quad i, j = 1, 2.$$

If the temperature field moves along the  $x_1$ -axis with constant velocity  $v$ , then, transforming the co-ordinates

$$(1.16) \quad \xi_1 = x_1 - vt, \quad \xi_2 = x_2,$$

Eq. (1.12) is reduced to

$$(1.17) \quad \left( \frac{v}{\kappa} \partial_1 + \frac{v^2}{c_1^2} \partial_1^2 \right) F_0(\xi_1, \xi_2) = -2\mu m [T(\xi_1, \xi_2) - S(\xi_1, \xi_2)],$$

where the functions  $T$  and  $S$  should satisfy the equation

$$(1.18) \quad \begin{cases} (\partial_1^2 + \partial_2^2 + v/\kappa \partial_1) T = -Q/\kappa, & \left( \partial_1^2 + \partial_2^2 - \frac{v^2}{c_1^2} \partial_1^2 \right) S = -Q/\kappa, \\ \partial_1 = \frac{\partial}{\partial \xi_1}, & \partial_2 = \frac{\partial}{\partial \xi_2}. \end{cases}$$

Let us observe that for an infinite elastic space Eq. (1.13) may also be obtained in another way.

Let us perform the Laplace transformation on Eqs. (1.7) and (1.4). We obtain the system of equations

$$(1.19) \quad (V^2 - p/\kappa) (V^2 - p^2/c_1^2) \tilde{F}_0 = -\frac{2\mu m}{\kappa} \tilde{Q},$$

$$(1.20) \quad (V^2 - p/\kappa) \tilde{T} = -\frac{\tilde{Q}}{\kappa}.$$

Let us perform on (1.19) the triple Fourier integral transformation determined by the equations

$$(1.21) \quad \begin{cases} f^*(a_r, p) = (2\pi)^{-3/2} \iint_{-\infty}^{\infty} \tilde{f}(x_r, p) e^{ia_r x_r} dV, & dV = dx_1 dx_2 dx_3, \\ \tilde{f}(x_r, p) = (2\pi)^{-3/2} \iint_{-\infty}^{\infty} f^*(a_r, p) e^{-ia_r x_r} dW, & dW = da_1 da_2 da_3. \end{cases}$$

The solution of (1.19) takes the form (2)

$$(1.22) \quad \tilde{F}_0(x_r, p) = -\frac{2(2\pi)^{-3/2}\mu m}{\kappa} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{Q^*(a_r, p) e^{-ia_r x_r} dW}{(a_r a_r + p/\kappa)(a_r a_r + p^2/c_1^2)}$$

or

$$(1.23) \quad \tilde{F}_0(x_r, p) = \frac{2(2\pi)^{-3/2}\mu m}{(p/\kappa - p^2/c_1^2)} \left\{ \frac{1}{\kappa} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{Q^* e^{-ia_r x_r} dW}{a_r a_r + p/\kappa} - \right. \\ \left. - \frac{1}{\kappa} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{Q^* e^{-ia_r x_r} dW}{a_r a_r + p^2/c_1^2} \right\}.$$

The first integral in figured brackets on the right-hand side of (1.23) is equal to  $\tilde{T}$ , as a solution of (1.20), the second may be treated as a solution of the differential equation

$$(1.24) \quad (\nabla^2 - p^2/c_1^2) \tilde{S} = -\frac{Q}{\kappa}, \quad S(x_r, 0) = \dot{S}(x_r, 0) = 0.$$

It should be added that for the determination of the function  $\tilde{F}_0$  it suffices to know the transforms of the function  $\tilde{T}$ . The function  $\tilde{S}$  will be obtained by replacing  $p/\kappa$  in the transform  $\tilde{T}$  by  $p^2/c_1^2$ .

Below a few solution examples are given for an infinite elastic space and an elastic layer.

## 2. The infinite space

Let an instantaneous linear source uniformly distributed along the  $x_3$ -axis act in the infinite space  $Q(x_r, t) = Q_0 \frac{\delta(r)}{2\pi t} \delta(t)$ . The resulting temperature field is

$$(2.1) \quad T(r, t) = \frac{Q_0}{4\pi\kappa t} \exp\left(-\frac{r^2}{4\kappa t}\right), \quad r^2 = x_1^2 + x_2^2.$$

On performing the Laplace transformation on Eq. (2.1), we obtain

$$(2.2) \quad \tilde{T}(r, p) = \frac{Q_0}{2\pi\kappa} K_0(r\sqrt{p/\kappa}),$$

where  $K_0(z)$  is the modified Bessel function of the third kind and of zero order.

Replacing  $p/\kappa$  in (2.2) by  $p^2/c_1^2$ , we obtain

$$(2.3) \quad \tilde{S}(r, p) = \frac{Q_0}{2\pi\kappa} K_0(rp\sigma), \quad \sigma = 1/c_1.$$

Therefore

$$(2.4) \quad \tilde{F}_0(r, p) = \frac{Q_0\mu m}{2\pi\kappa(p/\kappa - p^2/c_1^2)} [K_0(r\sqrt{p/\kappa}) - K_0(rp\sigma)].$$

On performing the inverse Laplace transformation, we obtain the function  $F_0$ . The same problem has been solved in another way by W. Derski [3].

In the case of a periodic source  $Q(x_r, t) = Q_0 e^{i\omega t} \frac{\delta(r)}{2\pi r}$ , we obtain from (1.14)

$$(2.5) \quad \Phi_0 = \frac{\mu m Q_0}{i\eta + k^2} [K_0(r\sqrt{i\eta}) - K_0(rk)], \quad \eta = \omega/\kappa, \quad k = \omega/c_1.$$

The stresses  $\sigma_{ij}$ , corresponding to the function  $\Phi_0$ , will be obtained from Eqs. (1.15)

Let the heat sources vary harmonically in time along the  $x_2$ -axis

$$Q(x_1, x_2, t) = Q_0 e^{i\omega t + ia_n x_2} \delta(x_1), \quad a_n = \frac{n\pi}{a}, \quad n = 0, \pm 1, \pm 2, \dots$$

In this case the following equation is to be solved

$$(2.6) \quad \nabla^2 U - i\eta U = -\frac{Q_0}{\kappa} \delta(x_1) e^{ia_n x_2}.$$

It is easy to verify that the following function is a solution of this equation

$$(2.7) \quad U = \frac{Q_0}{2\kappa} e^{ia_n x_2} \frac{e^{-\vartheta_n x_1}}{\vartheta_n}, \quad \vartheta_n = \sqrt{a_n^2 + i\eta}, \quad x_1 > 0.$$

Therefore

$$(2.8) \quad V = \frac{Q_0}{2\kappa} e^{ia_n x_2} \frac{e^{-\gamma_n x_1}}{\gamma_n}, \quad \gamma_n = \sqrt{a_n^2 - k^2}, \quad k = \omega/c_1, \quad x_1 > 0.$$

Substituting (2.7) and (2.8) into Eq. (1.14), we find

$$(2.9) \quad \Phi_0 = \frac{Q_0 \mu m}{\kappa (i\eta + k^2)} \left( \frac{e^{-\vartheta_n x_1}}{\vartheta_n} - \frac{e^{-\gamma_n x_1}}{\gamma_n} \right), \quad x_1 > 0.$$

Knowing  $\Phi_0$ , the stresses will be found from Eqs. (1.15).

### 3. The elastic layer

Let us consider an elastic layer of thickness  $2h$  with boundary surfaces free from stress. The same surfaces are heated harmonically in time according to the equation

$$(3.1) \quad T(\pm h, x_2, t) = e^{i\omega t} \sum_{n=-\infty}^{n=\infty} T_n e^{ia_n x_2} = \\ = e^{i\omega t} \left[ \frac{A_0}{2} + \sum_{n=1}^{\infty} (A_n \cos a_n x_2 + B_n \sin a_n x_2) \right], \quad a_n = n\pi/a.$$

In order to determine the particular integral  $F_0$  the following equation should be solved

$$(3.2) \quad \nabla^2 U - i\eta U = 0,$$

with the boundary conditions

$$(3.3) \quad U(h, x_2) = \sum_{n=-\infty}^{n=\infty} T_n e^{ia_n x_2} \quad \text{and} \quad U = 0 \quad \text{for} \quad x_1^2 + x_2^2 \rightarrow \infty.$$

The solution of Eq. (3.2) with the boundary conditions (3.3) has the form

$$(3.4) \quad U(x_1, x_2) = \sum_{n=-\infty}^{n=\infty} T_n \frac{\operatorname{ch} \vartheta_n x_1}{\operatorname{ch} \vartheta_n h} e^{ia_n x_2}, \quad \vartheta_n = \sqrt{a_n^2 + i\eta}.$$

Therefore

$$(3.5) \quad V(x_1, x_2) = \sum_{n=-\infty}^{n=\infty} T_n \frac{\operatorname{ch} \gamma_n x_1}{\operatorname{ch} \gamma_n h} e^{ia_n x_2}, \quad \gamma_n = \sqrt{a_n^2 - k^2},$$

and

$$(3.6) \quad \Phi_0 = \frac{2\mu m}{i\eta + k^2} \sum_{n=-\infty}^{n=\infty} T_n e^{ia_n x_2} \left( \frac{\operatorname{ch} \vartheta_n x_1}{\operatorname{ch} \vartheta_n h} - \frac{\operatorname{ch} \gamma_n x_1}{\operatorname{ch} \gamma_n h} \right).$$

Thus, a particular integral of Eq. (1.2) has been obtained, satisfying a part of the boundary conditions, the normal stresses  $\sigma_{11}$  on the boundaries  $x_1 = \pm h$  being zero. The shear stresses  $\sigma_{12}$  remain different from zero. To satisfy all the boundary conditions, particular integrals of (1.2) should be taken into consideration. Introducing the equation

$$(3.7) \quad F_1(x_r, t) = e^{i\omega t} \Phi_1(x_r), \quad F_2(x_r, t) = e^{i\omega t} \Phi_2(x_r),$$

Eq. (1.5) is reduced to the form

$$(3.8) \quad (\nu^2 + k^2) \Phi_1 = 0, \quad (\nu^2 + s^2) \Phi_2 = 0, \quad k^2 = \frac{\omega^2}{c_1^2}, \quad s^2 = \frac{\omega^2}{c_2^2}.$$

The solutions of these equations will be assumed in the form

$$(3.9) \quad \begin{cases} \Phi_1 = \sum_{n=-\infty}^{n=\infty} Q_n e^{ia_n x_2} \operatorname{ch} \gamma_n x_1, \\ \Phi_2 = \sum_{n=-\infty}^{n=\infty} b_n e^{ia_n x_2} \operatorname{ch} \beta_n x_1, \quad \beta_n = \sqrt{a_n^2 - s^2}. \end{cases}$$

From the boundary conditions  $\sigma_{12} = 0$ ,  $\sigma_{11} = 0$  for  $x_1 = h$ , that is from the conditions

$$(3.10) \quad -\Phi_{12} = 0, \quad \Phi_{22} + \frac{s^2}{2} \Phi = 0, \quad \Phi = \Phi_0 + \Phi_1 + \Phi_2,$$

the constants  $a_n$  and  $b_n$  can be determined. We find

$$(3.11) \quad \begin{cases} Q_n = \frac{2\mu m T_n}{i\eta + \sigma^2} \operatorname{ch} \beta_n h \frac{\vartheta_n \operatorname{th} \vartheta_n h - \gamma_n \operatorname{th} \gamma_n h}{\gamma_n \operatorname{sh} \gamma_n h \operatorname{ch} \beta_n h - \beta_n \operatorname{sh} \beta_n h \operatorname{ch} \gamma_n h}, \\ b_n = -a_n \frac{\operatorname{ch} \gamma_n h}{\operatorname{ch} \beta_n h}. \end{cases}$$

The knowledge of the function  $\Phi = \Phi_0 + \Phi_1 + \Phi_2$  will enable us to determine the stresses from the equations

$$(3.12) \quad \sigma_{ij} = e^{i\omega t} \left[ -\Phi_{,ij} + \delta_{ij} \left( V^2 + \frac{s^2}{2} \right) \Phi \right], \quad i, j = 1, 2.$$

Considerable simplification is obtained in the case of the boundary condition

$$(3.13) \quad T(\pm h, x_2, t) = T_0 e^{i\omega t},$$

where  $T$  does not depend on  $x_2$ . In this case the solution of the problem is confined to the function

$$(3.14) \quad F_0 = \frac{2\mu m T_0 e^{i\omega t}}{i\eta + k^2} \left( \frac{\operatorname{ch} x_1 \sqrt{i\eta}}{\operatorname{ch} \sqrt{i\eta} h} - \frac{\cos kx_1}{\cos kh} \right).$$

Making use of Eqs. (1.15) we find that the boundary conditions  $\sigma_{12} = 0$ ,  $\sigma_{11} = 0$  are satisfied here. The stresses in the elastic layer are

$$(3.15) \quad \sigma_{11} = -\frac{1}{2c_2^2} \ddot{F}_0, \quad \sigma_{22} = F_{0,11} - \frac{1}{2c_2^2} \ddot{F}_0, \quad \sigma_{12} = 0.$$

Thus, we have forced vibration produced by a harmonic temperature field. The excitation frequency  $\omega$  should not coincide with the natural vibration frequency of the layer  $\omega_n = \frac{2n-1}{2} \frac{\pi c_1}{h}$   $n = 1, 2, \dots, \infty$ . Otherwise we would have the phenomenon of resonance. The quantities  $\omega_n$  are the roots of the equation  $\cos kh = 0$ . For  $\omega$  approaching anyone of the  $\omega_n$  values, the stresses will increase indefinitely.

DEPARTMENT OF MECHANICS OF CONTINUOUS MEDIA, INSTITUTE OF FUNDAMENTAL TECHNICAL PROBLEMS, POLISH ACADEMY OF SCIENCES

(ZAKŁAD MECHANIKI OŚRODKÓW CIĘŻKICH, INSTYTUT PODSTAWOWYCH PROBLEMÓW TECHNIKI, PAN)

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